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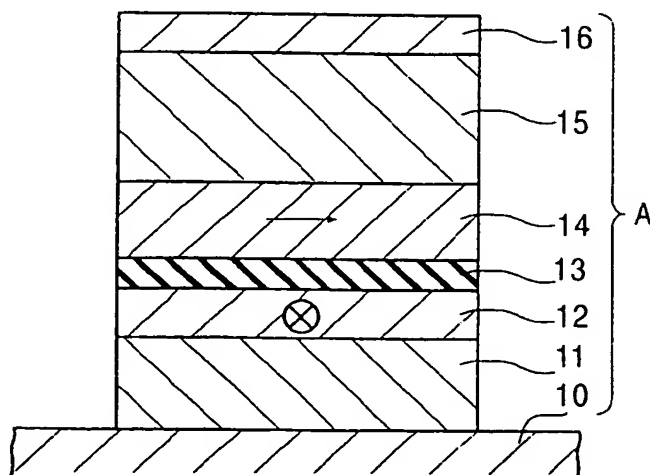
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(54) Magnetoresistive element

(57) The present invention provides a magnetoresistive element comprising at least one layer of a pinned ferromagnetic layer in which inversion of magnetization is pinned, at least one free layer of a free ferromagnetic layer magnetization of which freely rotates against the

external magnetic field and an auxiliary magnetization reversing layer positioned in adjoining or closely spaced relation to the free ferromagnetic layer to assist inversion of magnetization and having a soft magnetic characteristic, thereby enabling to lower the coercive force of the free ferromagnetic layer.

FIG. 1



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Description

The present invention relates to a magnetoresistive element constituting a magnetoresistive element used for magnetic heads, positioning sensors, rotation sensors and the like.

Conventional magnetoresistive reading heads (MR head) comprise AMR (Anisotropic Magnetoresistance) heads utilizing an anisotropic magnetoresistance phenomenon and GMR (Giant Magnetoresistance) heads utilizing a spin depending scattering phenomenon of conductive electrons, a spin-valve head that exhibit a high magnetoresistive effect at low external magnetic field being disclosed in the specification of US patent publication No. 5,159,513 as one example of GMR heads.

Fig. 9 is one example of the conventional spin-valve structure, which is constructed by laminating a free ferromagnetic layer 1, a nonmagnetic intermediate layer 2, a pinned ferromagnetic layer 3 and an antiferromagnetic layer 4 on a substrate, providing two magnet layers 5, 5 comprising Co-Pt and the like at both sides of this laminated member so as to insert the laminated member between the magnet layers, on which two electrode layers 6, 6 are provided.

In the conventional structure shown in Fig. 9, a relatively large bias magnetic field is needed to fix the direction of magnetization of the pinned ferromagnetic layer 3 along the z-direction in Fig. 9, a larger bias magnetic field being preferable. A bias magnetic field of at least 100 Oe is required in order to overcome an anti-magnetic field along the z-direction in Fig. 9 thereby preventing the direction of magnetization from being fluctuated due to a magnetic flux from a magnetic medium.

An exchange anisotropic magnetic field generated by providing a pinned ferromagnetic layer 3 in contact with an exchange coupling layer 4 is utilized in the conventional structure shown in Fig. 9 to obtain this bias magnetic field.

In the structure shown in Fig. 9, magnetization should be made to direct toward the track direction as a single magnetic domain by impressing a vertical bias parallel to the film face (X-direction in Fig. 9: the track direction) on the free ferromagnetic layer 1 from the magnet layers 5, 5, along with allowing the direction of magnetization of the pinned ferromagnetic layer 3 to direct toward the Z-direction in Fig. 9 as a single magnetic domain by impressing a bias along the Z-direction in Fig. 9, that is, a direction perpendicular to magnetization of the free ferromagnetic layer 1. The object of impressing a vertical bias is to suppress Barkhausen noise arising from a lot of magnetic domains formed by the free ferromagnetic layer 1 or, in other words, to make resistance against the magnetic flux from a magnetic medium to change smoothly with low noise levels.

The direction of magnetization of the pinned ferromagnetic layer 3 should not be changed by the magnetic flux (along the Z-direction in Fig. 9) from the magnetic

medium. Rather, a linear response could be obtained by allowing the direction of the free ferromagnetic layer 1 to change in a range of $90 \pm \theta^\circ$ relative to the direction of magnetization.

As described above, a magnetoresistive head having a good linear response in which Barkhausen noise is suppressed can be realized by taking advantage of a bias in the pinned ferromagnetic layer at the spin valve head, and the exchange anisotropic magnetic field generated in the vertical bias of the free ferromagnetic layer at a contact interface with the antiferromagnetic layer.

The exchange anisotropic magnetic field is a phenomenon arising from an exchange interaction between magnetic moments of the ferromagnetic layer and exchange coupling layer at a contact face between the two layers. An well known example of the antiferromagnetic layer that generate an exchange anisotropic magnetic field with a ferromagnetic layer, for example NiFe layer, is FeMn layer. However, corrosion resistance of FeMn layer is so poor that corrosion is progressed during the manufacturing process of magnetic heads or operation of magnetic heads, thereby largely deteriorating the exchange anisotropic magnetic field. While it is well known that the temperature at the position in closely spaced relation to the FeMn layer is easily increased to about 120°C due to heat generation by a steady sensing current, the exchange anisotropic magnetic field created by the FeMn layer is so sensitive to temperature changes that the exchange anisotropic magnetic field is approximately linearly reduced against temperature until it has been quenched at a temperature of about 150°C (a blocking temperature: T_b). Accordingly, there remains a problem that a stable exchange anisotropic magnetic field is hardly obtainable.

In USP 5,688,380, the inventors of the present invention disclosed a magnetoresistive element provided with a coercive force increasing layer of $\alpha\text{-Fe}_2\text{O}_3$ that is able to obtain a giant magnetoresistive effect besides having superior corrosion resistance and temperature characteristics to FeMn, wherein the element makes use of a mechanism in which pinning of rotation of magnetization is possible by increasing the coercive force of the ferromagnetic layer in adjoining relation thereto.

According to this patent application, a pinned ferromagnetic layer is formed by pinning rotation of magnetization of the ferromagnetic layer by disposing a coercive force increasing layer of $\alpha\text{-Fe}_2\text{O}_3$ to one of the two ferromagnetic layers laminated via non-magnetic layers while a free magnetic layer is formed by allowing magnetization of the other ferromagnetic layer to be freely rotated, thereby arising a resistance change by making the free ferromagnetic layer to rotate by the external magnetic field. Since the blocking temperature of $\alpha\text{-Fe}_2\text{O}_3$ is far more higher than that of FeMn, the magnetoresistive element having the structure described above has an advantage that its magnetic properties are hardly changed by temperature variations, characterized by having no problem in corrosion resistance be-

cause $\alpha\text{-Fe}_2\text{O}_3$ itself is an oxide.

Since the orientation of magnetization in the free ferromagnetic layer 1 of the free ferromagnetic layer 1 and pinned ferromagnetic layer 3 provided by inserting a non-magnetic layer 2 therebetween should be freely rotated by sensitively responding to the external magnetic field in the magnetoresistive element with a spin valve structure using FeMn, or in the magnetoresistive element provided with a coercive force increasing layer of $\alpha\text{-Fe}_2\text{O}_3$, it is preferable that the coercive force is small. On the contrary, the orientation of the pinned ferromagnetic layer 3 should not be made to move by responding to the external magnetic field.

In the structure in which the free ferromagnetic layer 1 and pinned ferromagnetic layer 3 are laminated via the non-magnetic layer 2, on the other hand, the coercive force of the free ferromagnetic layer 1 is increased higher than the inherent level of the material due to the effect of the magnetic field created by the pinned ferromagnetic layer 3, hindering free rotation of magnetization of the free ferromagnetic layer 1, so that characteristics of R-H curves as a magnetoresistive element may be possibly deteriorated.

The object of the present invention, which is carried out by taking the above situations into account, is to provide a magnetoresistive element being made easy to reverse magnetization as a result of low coercive force of the free ferromagnetic layer by providing with an auxiliary magnetization reversing layer and exhibiting a magnetoresistive effect sensitively responding to the external magnetic field, wherein the magnetoresistive effect can be prevented from being decreased by depressing the electric current that tends to be branched into the auxiliary magnetization reversing layer by providing the auxiliary magnetization reversing layer with a material of high resistivity.

For solving the hitherto described problems, the present invention is characterized by being provided with at least one pinned ferromagnetic layer in which inversion of magnetization is pinned, at least one free ferromagnetic layer in which magnetization is freely rotated against the external magnetic field, and an auxiliary magnetization reversing layer assisting inversion of magnetization of the ferromagnetic layer by being disposed in adjoining relation or in closely spaced relation to the free ferromagnetic layer and having an auxiliary magnetization reversing layer with soft magnetic characteristics.

It is preferable in the present invention that the auxiliary magnetization reversing layer mainly comprises a fine crystalline phase principally composed of bcc Fe structure and an amorphous phase containing an element M comprising one or a plurality of elements selected from Ti, Zr, Hf, V, Nb, Ta, W and rare earth elements, and O (oxygen).

It is preferable in the present invention that the auxiliary magnetization reversing layer mainly comprises a fine crystalline phase principally composed of bcc Fe

structure and a crystalline phase containing carbide and nitride of an element M' comprising one or a plurality of elements selected from Ti, Zr, Hf, V, Nb, Ta, W and rare earth elements.

According to the present invention, the pinned ferromagnetic layer is provided in adjoining relation to an exchange coupling layer so that inversion of magnetization of pinned ferromagnetic layer is pinned in response to the magnetic exchange coupling due to said exchange coupling layer.

The exchange coupling layer may be mainly composed of $\alpha\text{-Fe}_2\text{O}_3$ while the exchange coupling layer is mainly composed of a X-Mn alloy, wherein X in the composition formula X-Mn denotes one or a plurality of elements selected from platinum group elements.

It is preferable that the thickness of the auxiliary magnetization reversing layer is in the range of 50 to 300 Å and the specific resistivity of the auxiliary magnetization reversing layer is in the range of 200 to $2 \times 10^5 \mu\Omega\text{cm}$.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a cross section showing the 1st aspect of the magnetoresistive multilayer film according to the present invention.

Fig. 2 is a cross section showing the 2nd aspect of the magnetoresistive multilayer film according to the present invention.

Fig. 3 is a cross section showing the 3rd aspect of the magnetoresistive multilayer film according to the present invention.

Fig. 4 is a cross section showing the 4th aspect of the magnetoresistive multilayer film according to the present invention.

Fig. 5 is a graph indicating a M-H curve of a sample of the soft magnetic layer (a layer of $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$) provided on the Si substrate covered with a Al_2O_3 layer.

Fig. 6 shows a R-H curve of the free ferromagnetic layer of the magnetoresistive multilayer film having a laminated construction of Si substrate / Al_2O_3 layer / $\alpha\text{-Fe}_2\text{O}_3$ layer / NiFe layer / Cu layer / NiFe layer / $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ layer, and a R-H curve of the free ferromagnetic layer of the magnetoresistive multilayer film having a construction in which $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ layer is omitted in the foregoing laminated structure.

Fig. 7 shows a R-H curve of the free ferromagnetic layer of the magnetoresistive multilayer film having a laminated construction of Si substrate / Al_2O_3 layer / $\alpha\text{-Fe}_2\text{O}_3$ / NiFe layer / Co layer / Cu layer / Co layer / NiFe layer / $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ and a R-H curve of the free ferromagnetic layer of the magnetoresistive multilayer film having a construction in which the $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ layer is omitted in the foregoing laminated structure.

Fig. 8 shows a R-H curve of the free ferromagnetic layer of the magnetoresistive multilayer film having a laminated construction of Si substrate / Al_2O_3 layer / $\alpha\text{-Fe}_2\text{O}_3$ / NiFe layer / CoFe layer / Cu layer / CoFe layer

/ NiFe layer / $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ layer, and R-H curve of the free ferromagnetic layer of the magnetoresistive multilayer film having a construction in which $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ layer is omitted in the foregoing laminated structure.

Fig. 9 is a cross section of the 1st aspect of the conventional magnetoresistive sensor.

One embodiment of the present invention will be described hereinafter referring to the drawings, as an example

Fig. 1 is an aspect of a magnetoresistive multilayer film provided on the magnetoresistive element according to the present invention, wherein the magnetoresistive multilayer film A of this configuration is mainly composed of a substrate 10 of a non-magnetic member, and a pinning thin film layer 11, a pinned ferromagnetic layer 12, a non-magnetic layer 13, a free ferromagnetic layer 14, an auxiliary magnetization reversing layer 15 and a protective layer 16 each being laminated thereon.

While electrode layers and magnet layers to be used in the construction shown in Fig. 9 are omitted in Fig. 1, it is needless to say that the construction in Fig. 1 is also preferably applicable in the construction shown in Fig. 9 in order to allow resistance to be smoothly changed without any Barkhausen noise by impressing a vertical bias.

The substrate 10 is composed of a non-magnetic material represented by a glass, Si, Al_2O_3 , TiC, SiC and a sintered body of Al_2O_3 and TiC. A cover layer and a buffer layer may be appropriately provided on the substrate 10 for the purpose of eliminating roughness of the substrate surface or to make crystalline matching of the layer laminated thereon comfortable.

An exchange coupling layer 11 is provided in order to enhance coercive force of the pinned ferromagnetic layer 12 by allowing a magnetic exchange coupling force to effect on the pinned ferromagnetic layer 12 formed thereon. It is preferable that this exchange coupling layer 11 is composed of an antiferromagnetic material, especially an oxide antiferromagnetic material, an example of which being $\alpha\text{-Fe}_2\text{O}_3$. A hard magnetic material may be also used for this exchange coupling layer 11, an example of it being Co-Pt alloy and the like.

A magnetoresistive multilayer film being excellent in linear response in addition to being robust in temperature changes and securely suppressing Barkhausen noise can be provided if the exchange coupling layer 11 is composed of $\alpha\text{-Fe}_2\text{O}_3$ because the Molin point of $\alpha\text{-Fe}_2\text{O}_3$ itself is high.

The exchange coupling layer 11 can be also constructed with X-Mn alloy films (wherein X denotes one or a plurality of platinum group elements such as Pt, Pd, Ir, Ru and Rh).

Both of the pinned ferromagnetic layer 12 and free ferromagnetic layer 14 comprise ferromagnetic thin films, examples of them being NiFe alloy, NiCo alloy and NiFeCo alloy. The free ferromagnetic layer 14 and pinned ferromagnetic layer 12 can be composed of a NiFe alloy layers, respectively, or the free ferromagnetic

layer 14 may be constructed of a laminated structure of NiFe alloy layers or a laminated structure of CoFe alloy layers and NiFe alloy layers.

When the free ferromagnetic layer 14 is composed of a laminated structure, the layer is preferably made of a magnetoresistive multilayer film B in which a metallic layer 17 such as thin Co layer or CoFe ($\text{Co}_{90}\text{Fe}_{10}$) alloy is disposed to the non-magnetic layer 13 as shown in Fig. 2.

The reason of the above description comes from the fact that, with respect to the mechanism for generating a giant magnetoresistive effect arising from the structure in which the non-magnetic layer 13 is inserted between the ferromagnetic layers 12 and 14, a higher magnetoresistive effect can be obtained owing to a low possibility of arising a disturbing factor other than conductive electron spin depending scattering when the ferromagnetic layers 12 and 14 are composed of the same kind of material rather than composing the layer of different kind materials. From these facts, the structure shown in Fig. 2 in which the non-magnetic layer 13 side of the ferromagnetic layer 14 is replaced with a Co layer of a given thickness is preferable when the pinned ferromagnetic layer 12 is composed of Co. Also, Co may be predominantly contained in the non-magnetic layer 13 side of the ferromagnetic layer 14 to form an alloy, thereby forming a concentration gradient gradually decreasing Co concentration along the direction toward the auxiliary magnetization reversing layer 15, instead of especially providing a Co layer.

The non-magnetic layer 13 comprises a non-magnetic material represented by Cu, Cr, Au and Ag with a thickness of 20 to 40 Å. When the thickness of the non-magnetic layer 13 is less than 20 Å, the pinned ferromagnetic layer 12 becomes ready to be magnetically coupled with the free ferromagnetic layer 14. A thickness of more than 40 Å of the non-magnetic layer 13 is not preferable, on the other hand, because the effectiveness of conductive electrons that pass through the interface between the non-magnetic layer 13 and ferromagnetic layers 12 and 14 and arise magnetoresistive effect is decreased, or the magnetoresistive effect is diminished due to electric current branching effect.

The auxiliary magnetization reversing layer 15 comprises a soft magnetic material with small coercive force, large saturation magnetization, large magnetic permeability and large resistivity with a preferable thickness of 100 to 300 Å, examples of them being those having the following composition.

The preferable auxiliary magnetization reversing layer to be used in the present invention mainly composed of a fine crystalline phase principally comprising bcc Fe structure and an amorphous phase containing an element M comprising one or a plurality of elements of Ti, Zr, Hf, V, Nb, Ta, W and rare earth elements, and O (oxygen).

The auxiliary magnetization reversing layer also mainly comprises a fine crystalline phase principally

composed of bcc Fe structure and a crystalline phase containing carbides and nitride of an element M comprising one or a plurality of elements selected from Ti, Zr, Hf, V, Nb, Ta, W and rare earth elements.

Examples of the composition of these auxiliary magnetization reversing layer 15 are as follows.

Example of composition 1

A soft magnetic alloy represented by a composition formula $\text{Fe}_a\text{M}_b\text{O}_c$ can be applied in the present invention, wherein M denotes at least one element of the rare earth elements (Sc and Y belonging to 3A group of the periodic table, or lanthanoids such as La, Ce, Pr, Nd, Pm, Sm, Eu, Gd, Td, Dy, Ho, Er, Tm, Yb and Lu) or a mixture thereof, and the composition ratios a, b and c satisfy, preferably in atomic %, the relations of $50 \leq a \leq 70$, $5 \leq b \leq 30$, $10 \leq c \leq 30$ and $a + b + c = 100$. The soft magnetic alloys with this composition can be also used for the object of the present invention because they exhibit a high resistivity of the order of 400 to 1000 $\mu\Omega\cdot\text{cm}$ as shown in USP 5,573,863 disclosed by the inventors of the present invention.

Example of composition 2

A soft magnetic alloy represented by a composition formula $\text{Fe}_d\text{M}'_e\text{O}_f$ can be applied in the present invention, wherein M' denotes at least one element selected from a group of Ti, Zr, Hf, V, Nb, Ta and W or a mixture thereof, and the composition ratios d, e and f satisfy, preferably in atomic %, the relations of $45 \leq d \leq 70$, $5 \leq e \leq 30$, $10 \leq f \leq 40$ and $d + e + f = 100$. The soft magnetic alloys with this composition can be used for the object of the present invention because they exhibit a high resistivity of the order of 400 to $2.0 \times 10^5 \mu\Omega\cdot\text{cm}$ as shown in USP 5,573,863 disclosed by the inventors of the present invention.

Example of composition 3

The composition formula is represented by $\text{T}_{100-a'-b'-c'-d'}\text{M}'_{b'}\text{-Z}_{c'}\text{-Q}_{d'}$, wherein T represents any one or both of Fe and Co, X represents any one or both of Si and Al, M' represents at least one element selected from a group of Ti, Zr, Hf, V, Nb, Ta, Mo and W, Z represents any one or both of C and N, and Q represents at least one element selected from a group of Cr, Re, Ru, Rh, Ni, Pd, Pt and Au.

It is preferable that the foregoing composition satisfies the following composition ratio (atomic %): $0 \leq a' \leq 25$, $1 \leq b' \leq 7$, and $0.5 \leq c' \leq 10$.

The soft magnetic alloys with this composition can be used for the object of the present invention because they exhibit a high saturation magnetization density of more than 1T.

Example of composition 4

The composition formula is represented by $\text{T}_{100-a'-f'-b'-c'-d'}\text{Al}_f\text{M}'_{b'}\text{-Z}_{c'}\text{-Q}_{d'}$, wherein T represents any one or both of Fe and Co. M' represents at least one element selected from a group of Ti, Zr, Hf, V, Nb, Ta, Mo and W, Z represents any one or both of C and N, and Q represents at least one element selected from a group of Cr, Re, Ru, Rh, Ni, Pd, Pt and Au. It is preferable that the foregoing composition satisfies the following composition ratio (atomic %): $8 \leq e' \leq 15$, $0.5 \leq f' \leq 10$, $1 \leq b' \leq 7$, $0.5 \leq c' \leq 10$ and $0 \leq d' \leq 10$.

The soft magnetic alloys with this composition can be used for the object of the present invention because they exhibit a high saturation magnetization density of more than 1T.

Example of composition 5

The composition formula is represented by $(\text{Co}_{1-g}\text{T}_g)_x\text{M}_y\text{Q}_z\text{X}_w\text{Y}_s$, wherein T represents one or a plurality of elements selected from a group of Fe, Ni, Pd, Mn and Al, M represents at least one element selected from a group of Ti, Zr, Hf, Nb, Ta, M and Y, and one or a plurality of elements selected from rare earth elements, Q represents one or a plurality of elements selected from O, N and B, X represents one or both of Si and Cr, and Y represents one or both of Au and Ag. In the formula, g satisfies the relation of $0.05 \leq g \leq 0.5$ while y, z and w satisfy the relations of $3 \leq y \leq 30$, $7 \leq z \leq 40$, $0 \leq w \leq 20$ and $0 \leq s \leq 20$, respectively in atomic %, with a balance of inevitable impurities.

Through the protective layer 16 is provided for protecting the auxiliary magnetization reversing layer 15, the former layer can be omitted. An insulating overcoat layer may be also provided on this protective layer 16. It is preferable that the overcoat layer provided is composed of an insulating material such as Al_2O_3 and quartz.

In the construction shown in Fig. 1, a steady current is imparted to the magnetoresistive multilayer film A.

When the construction shown in Fig. 1 is provided, the orientation of magnetization in the pinned ferromagnetic layer 12 is pinned and the orientation of magnetization in the ferromagnetic layer 14 is made free in the area corresponding to the track width, so that a coercive force difference between the ferromagnetic layers 12 and 14 is created, thereby arising a giant magnetoresistive effect. That is to say, when an external magnetic field such as leakage magnetic field from a magnetic recording medium operates on the free ferromagnetic layer 14 whose rotation of magnetization has been made free, the orientation of magnetization of the free ferromagnetic layer 14 is easily rotated and a resistance change in the multilayer film with magnetoresistive effect is caused accompanied by the rotation, so that magnetic information recorded on the magnetic medium can be read.

Since an auxiliary magnetization reversing layer 15 having a large saturation magnetization and specific resistivity, and a small coercive force is provided on the free ferromagnetic layer 14 in the construction as described previously, the free ferromagnetic layer 14 can be coupled with the auxiliary magnetization reversing layer 15, thereby making it possible to reduce coercive force of the free ferromagnetic layer 14. The auxiliary magnetization reversing layer 15 is able to sensitively respond to the external magnetic field owing to its small coercive force besides magnetization of the free ferromagnetic layer 14 making a contact with the auxiliary magnetization reversing layer 15 is readily rotated since its saturation magnetization is large. Consequently, the magnetoresistive effect can be displayed with a good lineality. Since the auxiliary magnetization reversing layer 15 itself has a high specific resistivity, branching electric current being liable to flow through the auxiliary magnetization reversing layer 15 can be reduced, consequently increasing the proportion of current that flow through the interface between the non-magnetic layer 13 and ferromagnetic layers 12 and 14 to lower the reduced proportion of the magnetoresistive effect.

Since Cu and elements in the Ni-Fe alloy are ready to diffuse in the interface by a heat treatment in the construction in which the free ferromagnetic layer 14 comprising a Ni-Fe alloy (permalloy) is directly laminated on the non-magnetic layer 13 comprising Cu, heat resistance of the layer can be improved by providing a metallic layer 17 comprising Co or CoFe as shown in Fig. 2. The construction shown in Fig. 2 is preferable because the structure in which Co makes a contact with the non-magnetic layer exhibits a large magnetoresistive effect in the mechanism for generating magnetoresistive effect in which a non-magnetic layer of Cu is inserted into the ferromagnetic layers. However, since the metallic layer 17 tends to increase coercive force in the free ferromagnetic layer 14 in the construction shown in Fig. 2, the auxiliary magnetization reversing layer 15 provided on the free ferromagnetic layer 14 is effective because the former suppresses increase of the coercive force in the free ferromagnetic layer 14. Accordingly, the construction shown in Fig. 2 makes it possible to obtain a magnetoresistive multilayer film having a good heat resistance and large magnetoresistive effect besides allowing resistivity to change sensitively responding to the external magnetic field.

The exchange coupling layer 11 in the structure shown in Fig. 1 may be composed of α -Fe₂O₃, an oxide by itself, having a superior corrosion resistance to FeMn that is used in the conventional spin valve structure besides being characterized by its toughness to temperature variations due to its high Neel temperature.

The result of calculation of a sense current, a branch current fraction of the current that flows through the auxiliary magnetization reversing layer of the magnetoresistive multilayer film, is described below, wherein it is assumed that a coercive force increasing layer of

α -Fe₂O₃ with a thickness of 1000 Å, a pinned ferromagnetic layer of NiFe alloy with a thickness of 58 Å, a non-magnetic layer of Cu with a thickness of 22 Å and a free ferromagnetic layer of NiFe alloy with a thickness of 87 Å are laminated on the substrate and FeHfO films with a thickness of 50 Å, 100 Å and 200 Å, respectively, are formed thereon in the multilayer film A with a magnetoresistive effect.

Let the resistance of the spin valve structure portion comprising a pinned ferromagnetic layer, non-magnetic layer and free magnetic layer be R_{sv} , the electric current flowing therethrough be i_{sv} , the resistance of a auxiliary magnetization reversing layer be R_{OL} and the electric current flowing therethrough be i_{OL} . When a film with a composition of FeHfO (saturation magnetization $I_s = 1.4T$, specific resistivity $\rho = 380 \mu\Omega\text{-cm}$, coercive force $H_c = 0.4 \text{ Oe}$ and magnetic permeability μ' at 100 MHz = 1500) is used for the auxiliary magnetization reversing layer, i_{OL} 's can be calculated as 0.0089 i, 0.0177 i, 0.0348 i and 0.0514 i when the layer film thickness of the auxiliary magnetization reversing layers are 50 Å, 100 Å, 200 Å and 300 Å, respectively.

As shown Fig. 3, a magnetoresistive multilayer film C, for example with a trapezoidal cross section, is formed by laminating a pinned ferromagnetic layer 32, a non-magnetic layer 33, a free ferromagnetic layer 34, an auxiliary magnetization reversing layer 35 and a protective layer 36 in this order on a pinning thin film layer formed on a substrate constructing a magnetic head illustrated in the drawing, wherein two electrode layers 39, 39 inserting the magnetoresistive multilayer film C therebetween with a space corresponding the track width TW, and two magnetic layers 40, 40 that serve for allowing magnetization of the free ferromagnetic layer to be a single magnetic domain along X direction (the direction denoted by an arrow a in Fig. 3) are provided at both sides of the magnetoresistive multilayer film C.

In the construction described above, the directions of magnetization of free ferromagnetic layer 34 and magnetization of the pinned ferromagnetic layer 32 can be orthogonally aligned with each other with an angle of approximately 90° by allowing the former to direct along the direction of the arrow a in Fig. 3 and the latter to direct along the Z-direction.

The magnetoresistive multilayer film C with the construction shown in Fig. 3 is produced by the steps comprising: placing a non-magnetic ceramic substrate made of, for example, Al₂O₃ - TiC (Altic) in the chamber of a high frequency magnetron sputtering apparatus or an ion beam sputtering apparatus; replacing the atmosphere in the chamber with an inert gas such as Ar; and forming the layers in the required order. Targets required in forming the layers are, for example, α -Fe₂O₃ target, Ni-Fe target and Cu target.

The process for producing the magnetoresistive multilayer film A in Fig. 3 comprises: forming a pinning thin film layer 31 comprising α -Fe₂O₃ by sputtering on a substrate while impressing a magnetic field along the

Z direction in Fig. 1 in an reduced pressure of Ar of 3 mTorr or less; forming two ferromagnetic layers 32 and 34 with a non magnetic layer 33 inserted therebetween; and laminating an auxiliary magnetization reversing layer 35 and a protective layer 36 in this order. Then, the laminated layers are processed to form a magnetoresistive multilayer film C by removing the layers except the portion corresponding to the track width by a photolithographic process and ion milling. After forming the magnetoresistive multilayer film C, two magnetic layers 40 and 40, and two electrode layers 39 and 39 are formed so that the laminated member is inserted between the layers.

Subsequently, the direction of magnetization of the pinned ferromagnetic layer 32 is pinned to fix the direction of magnetization by applying a magnetic field perpendicular to the drawing paper in Fig. 3 to magnetize the pinning thin film layer 31.

A magnetoresistive sensor with a construction shown in Fig. 3 can be obtained by the foregoing treatment, wherein the direction of magnetization of the pinned ferromagnetic layer 32 and the direction of magnetization of the free ferromagnetic layer 34 are orthogonally aligned with each other with an angle of 90°. However, magnetization as described above is not necessary when the pinning thin film layer 31 is produced using ferromagnetic materials such as Fe-Mn, Pt-Mn and Ir-Mn, instead, the direction of magnetization of the pinned ferromagnetic layer 32 is pinned by an exchange coupling.

As shown in Fig. 4, the auxiliary magnetization reversing layer 15 in the magnetoresistive multilayer film A in Fig. 1 may be provided on the substrate 10, followed by providing a free ferromagnetic layer 14 thereon in addition to providing a pinned ferromagnetic layer 12 via a non-magnetic layer 13 in the present invention. An underlying layer may be also provided between the substrate 10 and auxiliary magnetization reversing layer 15, if necessary, to align the crystal orientation of the auxiliary magnetization reversing layer 15.

Fig. 5A and 5B show M-H curves when a soft magnetic film with a composition of $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ is used for the auxiliary magnetization reversing layer with a construction shown in Fig. 1. This auxiliary magnetization reversing layer is formed on a substrate of Si covered with a protective layer of Al_2O_3 with a thickness of 300 Å. Fig. 5A and 5B correspond to M-H curves along the hard axis of magnetization and easy axis of magnetization, respectively. The soft magnetic film of this composition exhibits an excellent M-H curve as a soft magnetic film.

Fig. 6A shows a R-H curve of the free ferromagnetic layer having a laminated construction of $\alpha\text{-Fe}_2\text{O}_3$ (coercive force increasing layer and pinning thin film layer, thickness 1000 Å) / NiFe layer (pinned ferromagnetic layer, thickness 58 Å) / Cu layer (non-magnetic layer, thickness 22 Å) / NiFe layer (free ferromagnetic layer, thickness 87 Å) / $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ (auxiliary magnetization

reversing layer, thickness 300 Å) on a substrate of Si substrate / Al_2O_3 layer, while Fig. 6B shows a R-H curve of the free ferromagnetic layer having a construction in which the auxiliary magnetization reversing layer is omitted in the foregoing laminated structure.

Fig. 7A shows a R-H curve of the free ferromagnetic layer having a laminated construction of $\alpha\text{-Fe}_2\text{O}_3$ (1000 Å) / NiFe layer (48 Å) / Co layer (10 Å) / Cu layer (22 Å) / Co layer (10 Å) / NiFe layer (77 Å) / $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ (300 Å) on a substrate of Si substrate / Al_2O_3 layer, while Fig. 7B shows a R-H curve of the free ferromagnetic layer having a construction in which the auxiliary magnetization reversing layer is omitted in the foregoing laminated structure. H_{cl} in the figure denotes the coercive force of the free ferromagnetic layer.

Fig. 8A shows a R-H curve of the free ferromagnetic layer having a laminated construction of $\alpha\text{-Fe}_2\text{O}_3$ (1000 Å) / NiFe layer (48 Å) / CoFe layer (10 Å) / Cu layer (22 Å) / CoFe layer (10 Å) / NiFe layer (77 Å) / $\text{Fe}_{60}\text{Hf}_{10}\text{O}_{30}$ (300 Å) on a substrate of Si substrate / Al_2O_3 layer, while Fig. 8B shows a R-H curve of the free ferromagnetic layer having a construction in which the auxiliary magnetization reversing layer is omitted in the foregoing laminated structure. H_{cl} in the figure also denotes the coercive force of the free ferromagnetic layer as in Fig. 6.

It is made clear from the results in Fig. 6, Fig. 7 and Fig. 8 that coercive force (H_{cl}) becomes smaller in each laminated structure in each sample provided with the auxiliary magnetization reversing layer than the samples without this layer. Accordingly, inversion of magnetization is made easy by a small external magnetic field in the magnetoresistive multilayer film provided with an auxiliary magnetization reversing layer, sensitively responding to the external magnetic field.

Claims

1. A magnetoresistive element comprising at least one pinned ferromagnetic layer in which inversion of magnetization is pinned, at least one free ferromagnetic layer in which magnetization is freely reversed in response to external magnetic field, and an auxiliary magnetization reversing layer assisting inversion of magnetization of the free ferromagnetic layer in adjoining relation or closely spaced relation to the free ferromagnetic layer and having a soft magnetic characteristic.
2. A magnetoresistive element according to Claim 1, wherein said auxiliary magnetization reversing layer mainly comprises a fine crystalline phase principally composed of bcc Fe structure and an amorphous phase containing an element M comprising one or a plurality of elements selected from Ti, Zr, Hf, V, Nb, Ta, W and rare earth elements, and O (oxygen).

3. A magnetoresistive effect element according to Claim 1, wherein said auxiliary magnetization reversing layer mainly comprises a fine crystalline phase principally composed of bcc Fe structure and a crystalline phase containing carbide or nitride of an element M comprising one or a plurality of elements selected from Ti, Zr, Hf, V, Nb, Ta, W and rare earth elements. 5
4. A magnetoresistive element according to Claim 1, 2 or 3, wherein said pinned ferromagnetic layer is provided in adjoining relation to an exchange coupling layer so that inversion of magnetization of pinned ferromagnetic layer is pinned in response to the magnetic exchange coupling due to said exchange coupling layer. 10 15
5. A magnetoresistive element according to Claim 4, wherein said exchange coupling layer is mainly composed of α -Fe₂O₃. 20
6. A magnetoresistive element according to Claim 4, wherein said exchange coupling layer is mainly composed of a X-Mn alloy (wherein X in the composition formula X-Mn denotes one or a plurality of elements selected from platinum group elements). 25
7. A magnetoresistive element according to any one of Claims 1-6, wherein the thickness of said auxiliary magnetization reversing layer is in the range of 50 to 300 Å. 30
8. A magnetoresistive element according to any one of Claims 1-7, wherein the specific resistivity of said auxiliary magnetization reversing layer is in the range of 200 to $2 \times 10^5 \mu\Omega\text{cm}$. 35

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FIG. 1

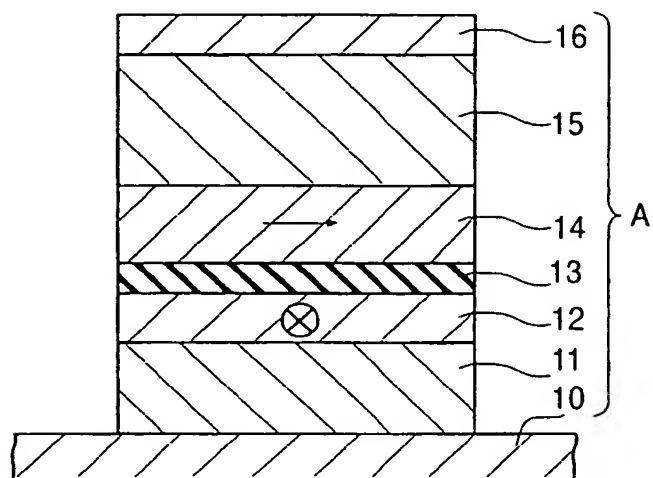


FIG. 2

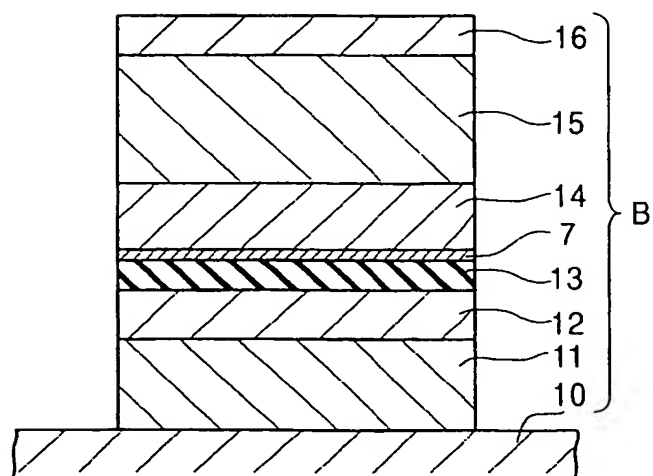


FIG. 3

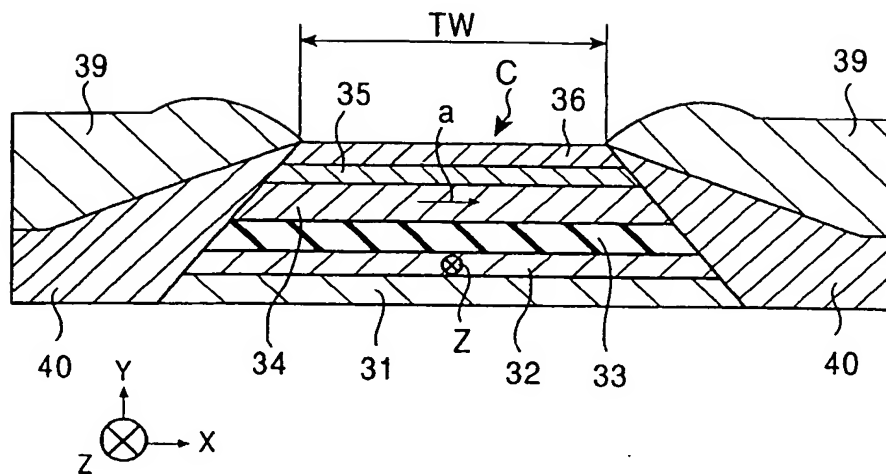


FIG. 4

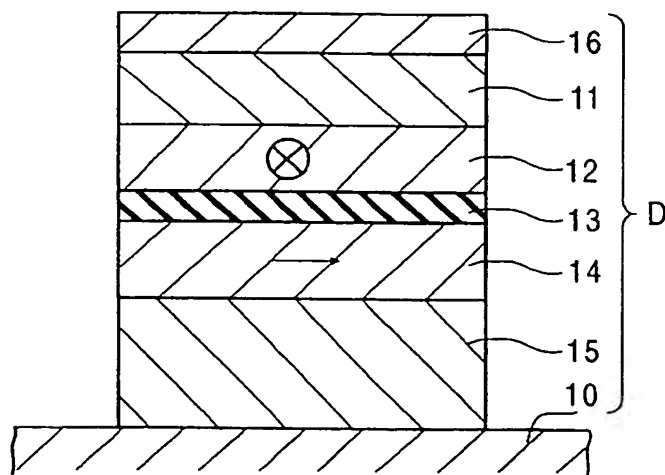


FIG. 5

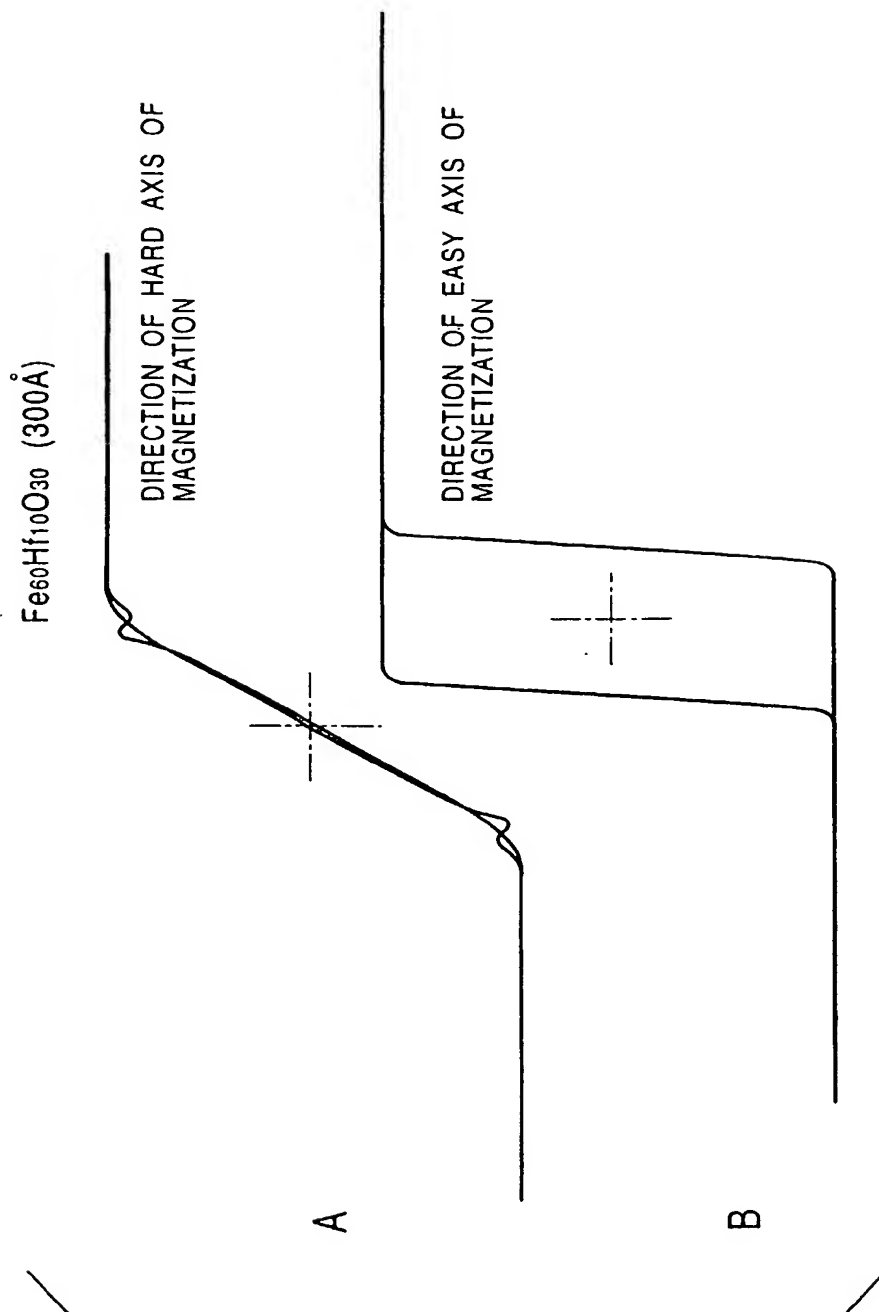


FIG. 6

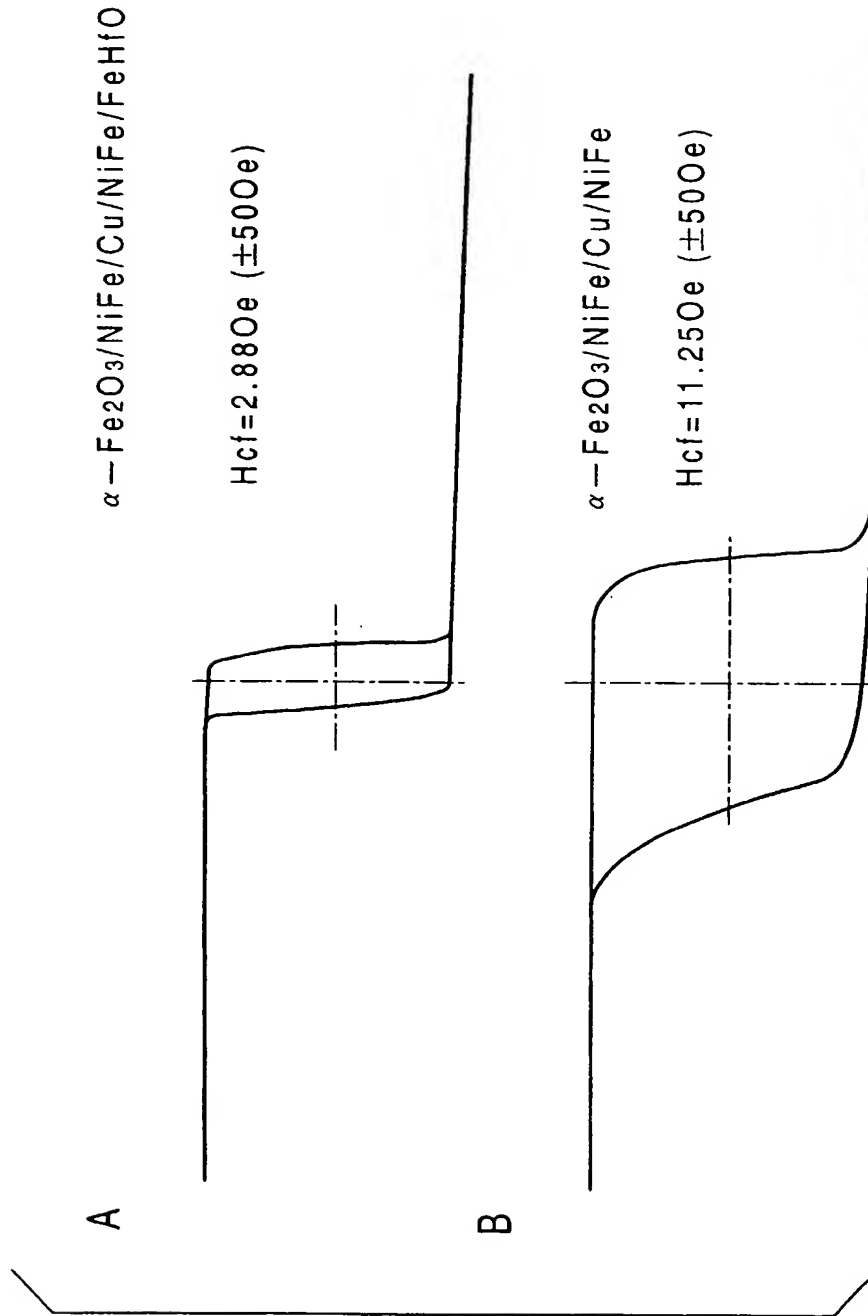


FIG. 7

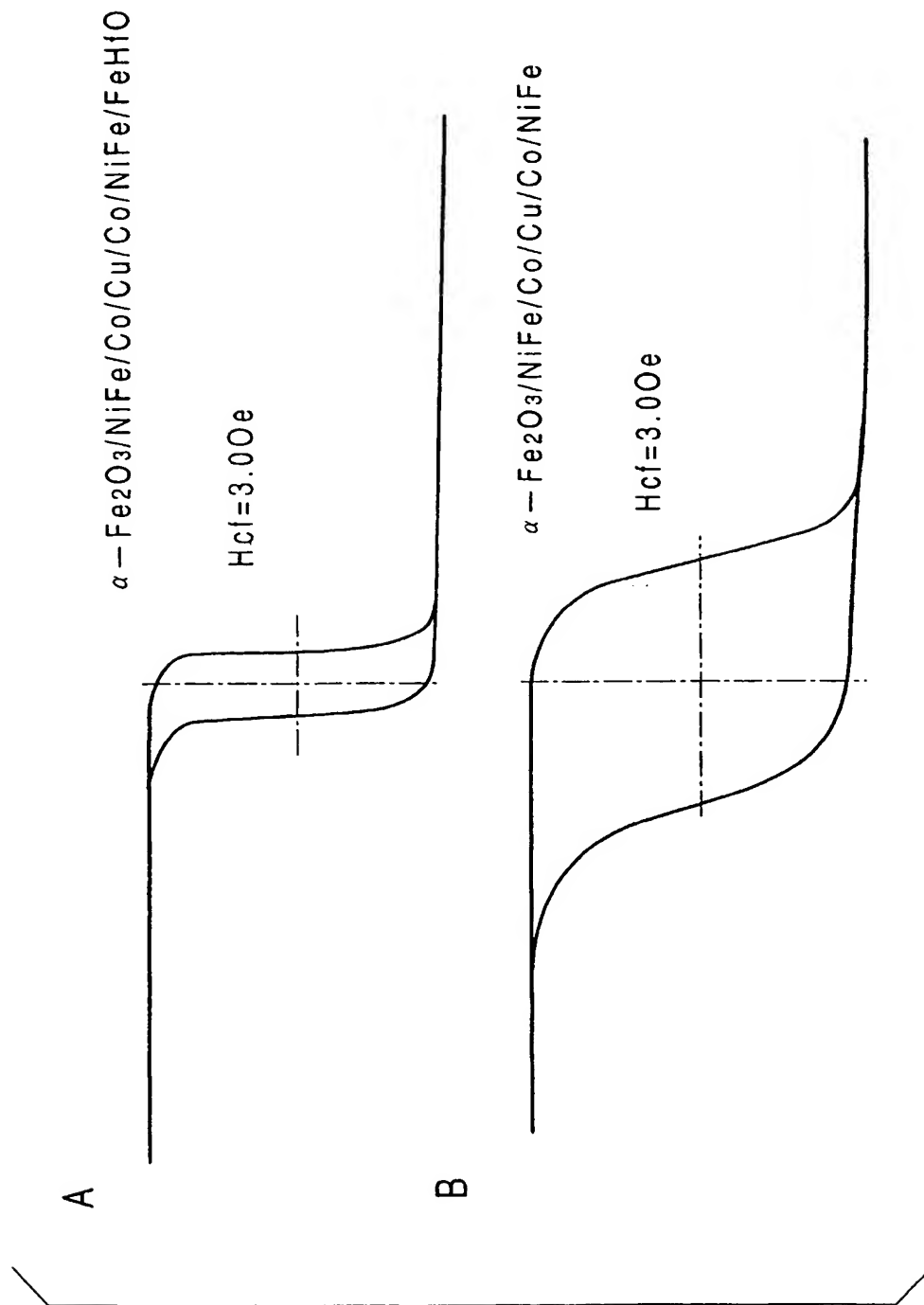


FIG. 8

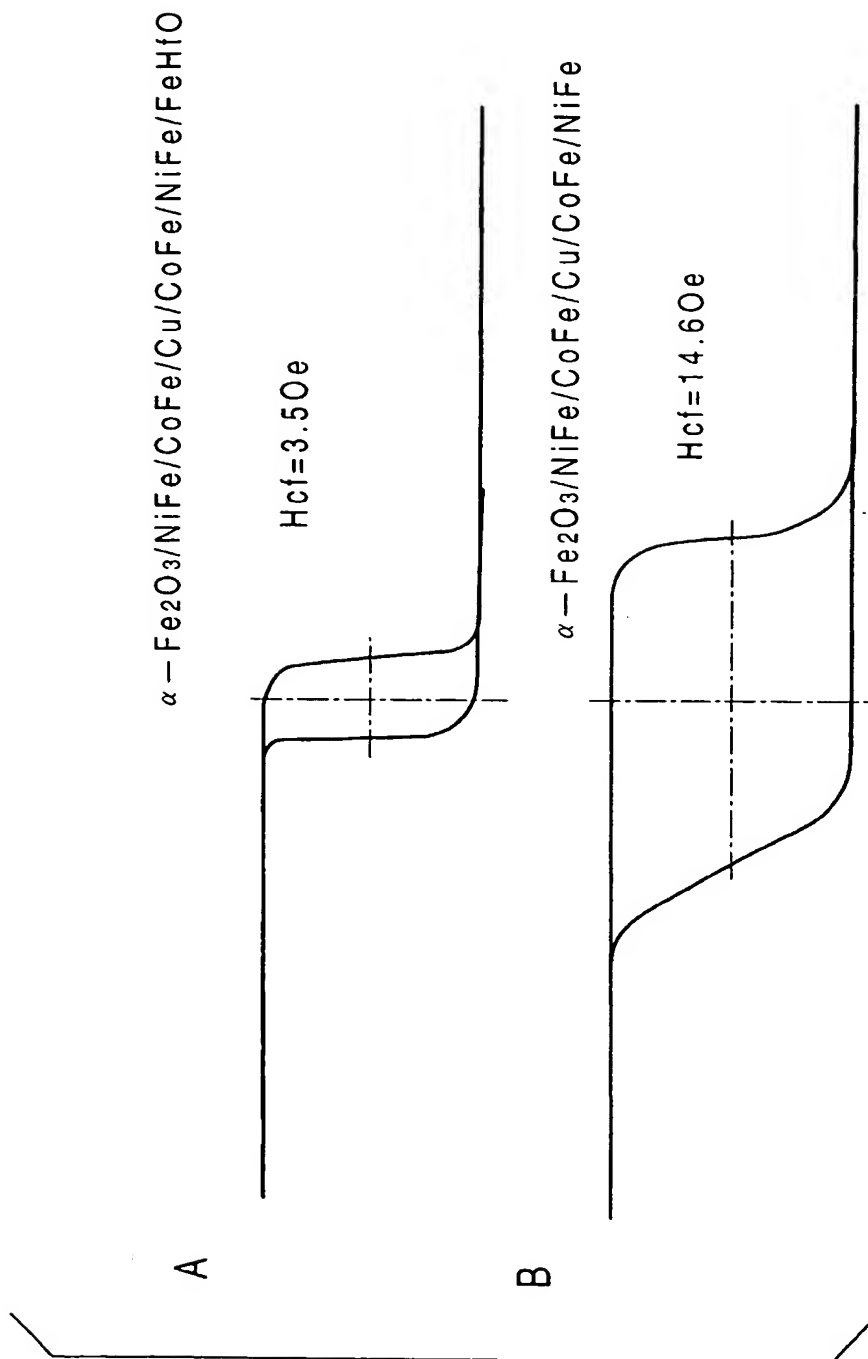
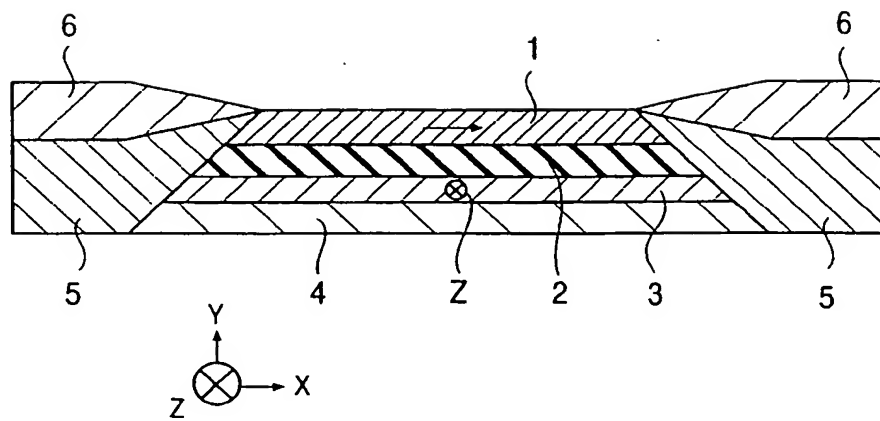


FIG. 9





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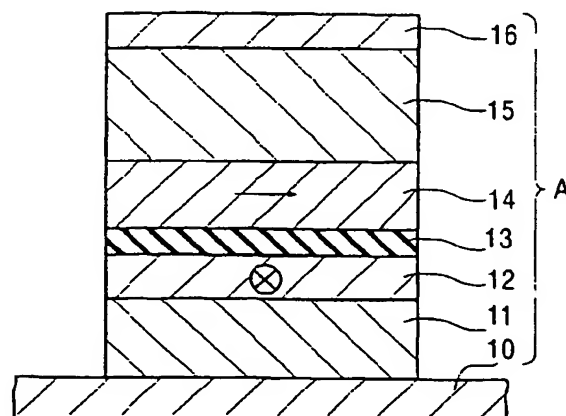
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(54) **Magnetoresistive element**

(57) The present invention provides a magnetoresistive element comprising at least one layer of a pinned ferromagnetic layer in which inversion of magnetization is pinned, at least one free layer of a free ferromagnetic layer magnetization of which freely rotates against the

external magnetic field and an auxiliary magnetization reversing layer positioned in adjoining or closely spaced relation to the free ferromagnetic layer to assist inversion of magnetization and having a soft magnetic characteristic, thereby enabling to lower the coercive force of the free ferromagnetic layer.

FIG. 1



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EUROPEAN SEARCH REPORT

Application Number
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DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
A	TSUNASHIMA S ET AL: "SPIN VALVES USING AMORPHOUS MAGNETIC LAYERS" JOURNAL OF MAGNETISM AND MAGNETIC MATERIALS, vol. 165, no. 1/03, January 1997, pages 111-114, XP000641748 * the whole document *	1, 2, 4, 8	H01L43/08 G01R33/09 G11B5/39 H01F10/08
A	EP 0 674 327 A (NIPPON ELECTRIC CO) 27 September 1995 * claims 1,3 *	1, 4-6	
A	EP 0 373 615 A (MATSUSHITA ELECTRIC IND CO LTD) 20 June 1990 * page 3, line 1 - line 5; claims 1,3 *	1, 3	
D, A	US 5 573 863 A (HAYAKAWA YSUO ET AL) 12 November 1996		
			TECHNICAL FIELDS SEARCHED (Int.Cl.6)
			H01L G01R G11B H01F
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 6 April 1999	Examiner Decanniere, L
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Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP 0674327 A	27-09-1995	JP 2785678 B	13-08-1998
		JP 7262529 A	13-10-1995
		DE 69502865 D	16-07-1998
		DE 69502865 T	18-03-1999
		US 5849422 A	15-12-1998
EP 0373615 A	20-06-1990	JP 2263416 A	26-10-1990
		JP 2263409 A	26-10-1990
		JP 2163911 A	25-06-1990
		US 5028280 A	02-07-1990
US 5573863 A	12-11-1996	JP 6316748 A	15-11-1994

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